

Influence of Penstock Outlet, Number of V-Blades, Flat Blade Lateral Twist Angle and Hub to Blade Ratio on the Performance of a Simplified Pico Hydropower System

By Alex Okibe Edeoja^{*}, Matthew Ekoja[†] & Taofeek A. Yusuf[‡]

A study to determine the influence of penstock outlet, number of v-blades, flat blade lateral twist angle and the hub to blade ratio on the performance of the Pico-hydro system has been conducted. Five turbine runners with 8, 9, 10, 11 and 12 v-blades were fabricated and tested on an already existing system. A runner with adjustable flat blades was also fabricated and tested for twist angles of 50^o, 55^o, 60^o, 75^o and 90^o. Runners with v-blades but having hub to blade ratios of 0.3, 0.4, 0.55, 0.65 and 0.7 were also tested. The turbine was connected to 3.9 kVA alternator via a v-belt drive and a 1 Hp pump was used to sustain the flow. The turbine and alternator shaft speeds were measured, and the level of water in the overhead and underground reservoirs monitored. The flow rate, available head and the hydraulic power were computed for each operation. The results obtained indicated that using a combination of a runner with 12 blades and a penstock outlet of 20 mm, 0.55 hub to blade ratio and lateral twist angles greater than 75^o combined with penstock outlets larger than 20 mm have the potentials of better performance in terms of power generation. The results of correlation and reliability test using Cronbach's alpha carried out on the data at 95% confirmed these findings. This will be very useful for further development of the system in order to attain implementable status as a clean and decentralized energy source.

Keywords: Blade Lateral Twist Angle, Hub to Blade Ratio, Number of Blades, Pico Hydro, Penstock Outlet.

Introduction

The challenge of the 21st century is how to develop sustainably and maintain the quality of life for a growing population with higher expectations for wellbeing. Underlying this challenge is the need for sufficient and sustainable supplies of energy to provide the economic activity underpinning these expectations. The measure of development in any society is synonymous with the level of energy consumption (British Petroleum 2017, Newell and Phillips 2016, SEP 2013, ECA 2014, Edeoja et al. 2015a). Energy plays the most vital role in the economic growth, progress, and development, as well as poverty eradication and security of any nation. Uninterrupted energy supply is a vital issue for all countries today (Obande et al. 2017, Arto et al. 2016, Lajqi et al. 2016, MDGs 2015, UNDESA 2014). Future economic growth crucially depends on the long term availability of

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energy from sources that are sustainable, affordable, accessible, and environmentally friendly. It is noted that the standard of living of a given country can be directly related to the per capita energy consumption, as the per capita energy consumption is a measure of the per capita income as well as a measure of the prosperity of a nation (Lipu et al. 2017, Shittu 2015, WHO 2015, Portale and de Wit 2014, Bergasse et al. 2013, Saatci and Dumrul 2013, Pirlogea and Cicea 2012, Lior 2010).

World Energy Council (2013) addressed the main factors that have influenced the development of the global energy sector the most over the previous two decades adding that the world has changed significantly in this period. The council summarized the principal drivers that have shaped energy supply and use to include sharp increase in the price of oil since 2001, financial crisis and slow economic growth with drastic reduction in energy consumption in large economies, shale gas in North America, the Fukushima Daiichi nuclear accident and the volatile political situation in the energy supplying countries in the Middle East and North Africa. Others are lack of global agreement on climate change mitigation, collapse of CO₂ prices in the European Emissions Trading System, exponential growth in renewables, deployment of 'smart' technologies, energy efficiency potential still remaining untapped, and growing public concern about new infrastructure projects, including energy projects (Samy 2017, Hossain et al. 2017, Choi et al. 2017).

Currently, the global energy demand is rising fast as population and emerging economies like China and India are growing exponentially with small and medium enterprises springing up. In developing countries of Africa like Nigeria, the International Energy Agency forecasts that energy demand would be 50% higher in 2030 than they are today (British Petroleum 2017, British Petroleum 2016, UNIDO, 2010, Sambo 2008a, Sambo 2008b, IEA 2007). Yet fossil fuels on which the world mostly depends are finite and are not environmentally friendly (Akuru and Okoro 2011, Williams and Alhaji 2003). There is therefore a gradually shifting of attention to potential renewable energy resources for power generation like wind, solar and hydro power resources. Renewable energy constitutes about 15% of the world's energy mix with hydropower making most of it (REN21 2016, UNFCCC 2015, REN21 2014, Bala 2013a, Bala 2013b, UNIDO 2009).

Access to electricity is a prime key to development as it provides light, heat and power for productive uses and communication, and the global demand keeps growing. A vast majority of the people in developing countries, especially in rural areas, do not have access to electricity (IEA 2015, Shezi 2015, Yuksel et al. 2013, Sambo 2005). This number keeps increasing despite the rural electrification programs because they are not sufficient to cope with the population growth or the political will in some of the places is not strong enough or absent (Omprasad 2016, Ramos et al. 2012, Adejumobi et al. 2013, Wang 2009). Moreover, despite the fact that about 80% of the world's population lives in developing countries, they consume only about 20% of the global commercial energy. According to the World Bank, most of the world's poor people spend more than 12% of their total income on energy, which is much more than what a middle-income family in the developed world spends (World Bank 2008, World Bank 2006).

Studies have indicated that about 40% Nigerian households have access to the national grid with more than 45% not having access to any form of electricity. About 6% have supported their access to the grid with standby generators and more than 3% completely relied on them. Also, about 1.1% of households have access to the rural electrification programs while a vast majority of Nigerians still use firewood for cooking with about 20% relying on kerosene. This is a direct consequence of low access to and low reliability of electricity services. These findings show the urgent need for efforts for further developments of the overall Nigerian electricity sector as well as rural electrification programs to ensure rapid economic development (Edomah 2016, Adejumobi et al. 2013, Oseni et al. 2012, Sambo 2008c). There is a need to revolutionize the way energy is produced and used to reduce these impacts while providing energy services to the billions of people who have inadequate or no access to electricity (Shezi 2015, Mustonen et al. 2010). Population growth makes the challenge even harder. The energy revolution will require moving from electricity systems based on large-scale fossil fuels, large hydro and nuclear fission plants to the ones based on new renewable sources and massive improvements in the efficiency of production, transportation, and storage and use of energy (Kumar and Biswas 2017, Okonkwo et al. 2017, Paun and Paun 2017, Ribal et al. 2017, Nguyen et al. 2016).

Water is the better choice among renewable sources because a small-scale hydropower is a relatively very cost-effective and reliable energy technology to be considered for providing clean electricity generation (Liu et al. 2013a, Liu et al. 2013b). Hydropower is a renewable, economical, non-polluting and environmentally benign. It accounts for about 19% of global electricity production from both large and small power plant second only to fossil fuels (Adamkowski 2012, Gatte and Kadhim 2012, Mishra et al. 2011a, Mishra et al. 2011b). The world has endless potential for hydropower generation. A lot of hydropower stations have been built all over the world and many more projects with a capacity above 100, 000 MW currently going on globally. Asia has the largest contribution of around 84, 000 MW (Nikolaisen 2015, Kaunda et al. 2012). In Nigeria, the potential is about 14,750 MW of power. About 1980 MW of this potential has been explored at Kainji, Jebba and Shiroro hydropower stations, leaving 12,200 MW unexplored (Bala 2013b, Adejumobi et al. 2013, Ohunakin et al. 2011, Olusegun et al. 2010). This implies that only about 14% of the nation's hydropower potential is in use. This inability to exploit its vast hydropower potential and to the fact that the available large hydropower plants are not operating up to installed capacity has negatively impacted power supply in Nigeria (Olukanmi and Salami 2012, Akuru and Okoro 2011). The present government has resuscitated interest in developing the project at Mambilla plateau in a bid to tackle part of the power supply problem.

Hydroelectric power plants despite having many advantages over other energy sources, have potentially negative environmental and socio-economic impacts (Nikolaisen 2015, Finardi and Suzzanto 2013, Hussey and Pittock 2012, Islar 2012). It is not a reliable source of energy because it depends on the hydrological cycle. Also, global climate change will increase rainfall variability and unpredictability, translating to more unpredictability, and increased flooding due to global warming is a big hazard to the safety of dams (Cunbin et al. 2012,

Jia-kun 2012, Jager 2008). Furthermore, reservoirs lose storage capacity to sedimentation which can diminish the capacity of dams to generate power. Hydropower projects also alter the habitats of aquatic organisms and affect them directly (Baumann and Stevanella 2012, Deng et al. 2012, Deng et al. 2011, Liu et al. 2012, Fjeldstad et al. 2012, Horlacher et al. 2012). Millions of people have been relocated from their homes to make way for dams, losing their land, livelihoods and access to natural resources and enduring irreparable harm to their cultures and communities (Melikoglu 2013, Bohlen and Lewis 2009). There is also growing evidence suggesting that reservoirs emit significant quantities of greenhouse gases especially in the lowland tropics (Chanudet et al. 2012, Cheng et al. 2012, Amor et al. 2011, Liu et al. 2011, Miller et al. 2011). Also, hydropower is often falsely promoted as cheap and reliable, projects are prone to cost overruns and often do not produce as much power as predicted (Aslani 2013, Goodland 2010, Sternberg 2010). The foregoing demerits are more directly applicable to large hydropower schemes which inform the need to resort to smaller schemes (mini, micro and Pico). They have continued to gain increasing popularity especially in remote areas due to design simplicity, ease of operation and relatively low environmental impacts (Wohlgemuth 2014, Pascale et al. 2011). Furthermore, communities could take advantage of simple drinking water projects or irrigation systems to install small hydro schemes.

Pico-hydro power provides a very good option for applying the advantages of hydropower while minimizing the operational and natural shortcomings. It suits the general requirements of smarter, smaller and decentralized systems, generating up to 5 kW. It has become a very useful option in Asian developing countries where the topography inhibits the uptake of more conventional grid-connected energy systems (Nimje and Dhanjode 2015, Xuhe et al. 2014, Haidar et al. 2012, Alexander et al. 2009a, Alexander et al. 2009b, Chuenchooklin 2006, Maher et al. 2003). Over the last 30 years it has been proven as a cost effective, clean and reliable method of generating electricity and mechanical power for off-grid applications and will play an important role in rural electrification into the foreseeable future. In Nepal, as at 2013, about 300 Pico hydro schemes constructed by Practical Action are producing electricity while 900 others are used for mechanical power only (Cobb and Sharp 2013).

There are many sites suitable for Pico hydro development in Nigeria as in many other African countries. Pico hydro has made some inroads in sub Saharan Africa as well, where electrification rates are some of the world's lowest (Wang 2009). However, focus has not been given to it as part of frantic efforts to combat the energy crisis (Bala 2013b, Ajuwape and Ismail 2011). This could be most likely as a result the desire in developing countries for executing gigantic projects which most often become moribund. If fully utilized, it would contribute remarkably to reducing the energy problems of domestic and commercial consumers in addition to providing a cheap source of power to remote areas where the extension of grid system is comparatively uneconomical (Adejumobi et al. 2013, Cobb 2011, Olusegun et al. 2010).

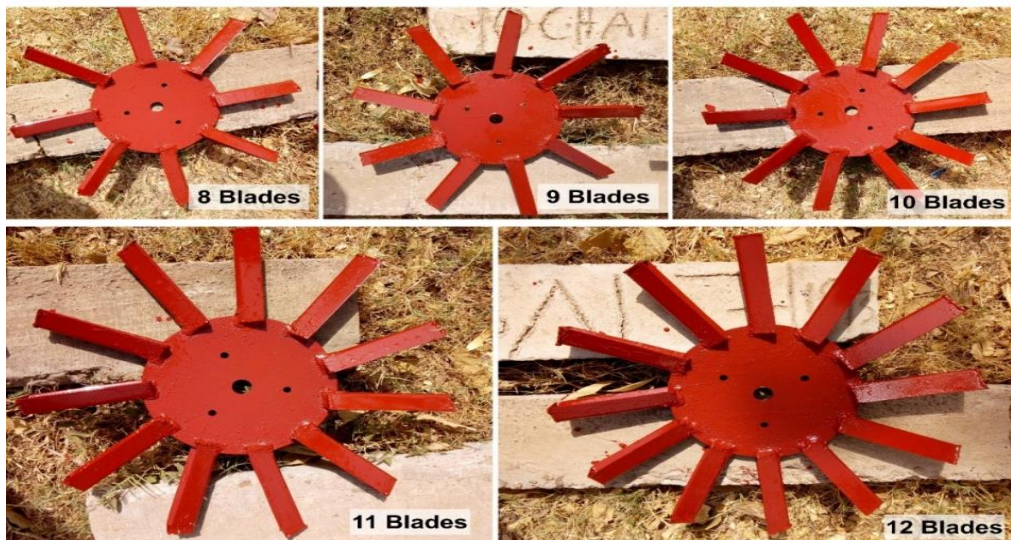
Pico hydro systems are not prone to sabotage and terrorist attacks as individuals and communities take responsibility of safeguarding their own

facilities. Due to the increased rate of terrorist activity in the country, the need and use for small Pico hydro is more attractive as power can be generated within the domestic environment, hence increasing energy security since generation and distribution are simplified (Othman et al. 2015, Alexander and Giddens 2008a, Alexander and Giddens 2008b, Williams 2007). While presenting significant advantages, its implementation has several challenges including a heavy dependence on site specific conditions for scheme design. Moreover, seasonal fluctuations of water levels also affect the operation of the conventional Pico hydro schemes, and low water levels do not allow optimal operation while very high ones can sweep the units away (Lahimer et al. 2012). Off the shelf systems have been designed to reduce the site specific requirement but the need for technical expertise and periodic maintenance still remains (Alexander and Giddens 2008a, Maher 2002a, Maher 2002b, Maher and Smith 2001). To further reduce the cost of the technology standard pumps and induction motors could be used in place of conventional generators and turbines (Smith and Williams 2003).

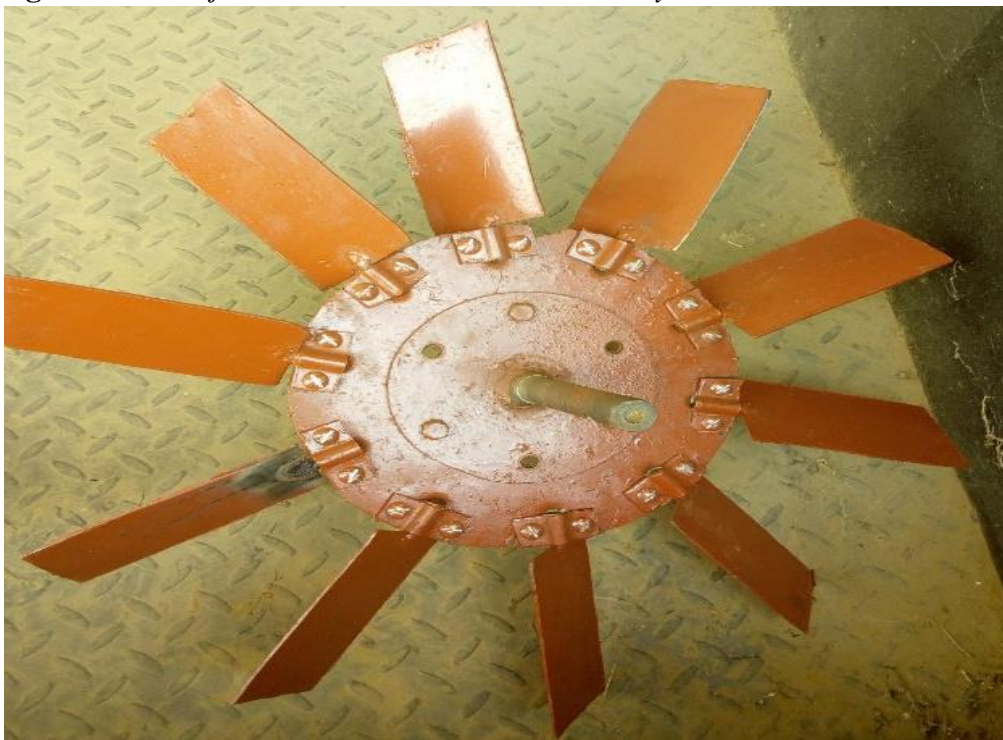
This study however focuses on the investigation of the effect of penstock outlet, turbine blade to hub ratio, the number of V-blades and the lateral twist angle of flat blades on the performance of a simplified Pico hydropower system that has been undergoing development in the Department of Mechanical Engineering, University of Agriculture, Makurdi, Nigeria, for about four years now (Edeoja and Awuniji 2017, Edeoja et al. 2017, Ipilakyya et al. 2017, Edeoja et al. 2016a, 2016b, 2016c, 2015b). It basically involves an overhead water reservoir with a locally fabricated turbine at its foot and has an underground reservoir. A pump is used for recycling the water, PVC pressure pipes as penstocks, tapered pipes as penstock outlets and an alternator. The present development will explore all the merits of Pico hydro systems while giving control to the user and as result minimize exposure to sabotage as well as bringing the benefits of hydropower to locations without natural water sources for conventional schemes. This particular aspect will further strengthen the prospects of eventually implementing this system for the end user small energy needs.

Methodology

The fabrication of the basic components of the system was done in the Mechanical Engineering workshop of the Federal University of Agriculture, Makurdi, Nigeria. Three parameters, number of v-blades, flat blade lateral twist angle and hub to blade ratio were studied with varying penstock outlets as part of an ongoing work. The runner with v-blades comprised of a circular hub with blades welded around its periphery. The diameter of the runners as well as the hub to blade ratio was obtained from Edeoja et al. (2015b). All the hubs and blades were fabricated from a 2 mm and 1.5 mm thickness mild steel sheet respectively. Five sets of runners were fabricated with 8, 9, 10, 11 and 12 blades. The runner assemblies are shown in Figure 1.

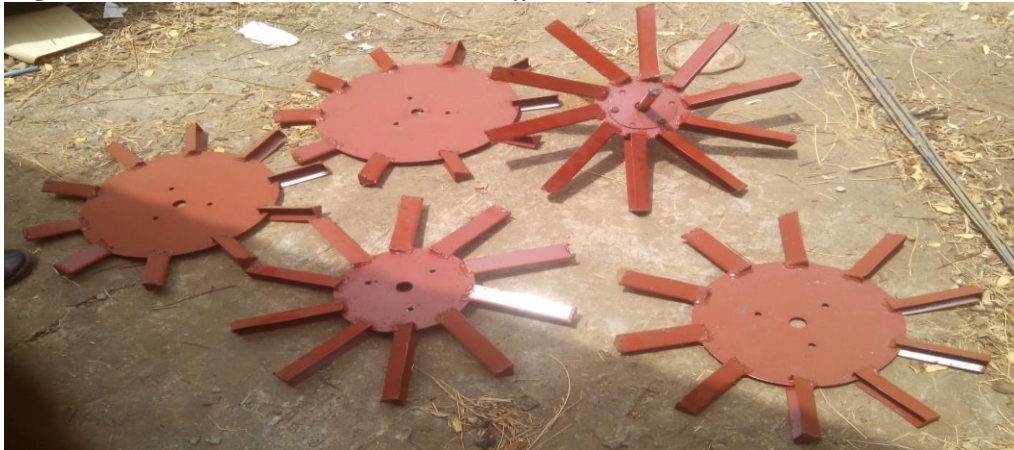
Figure 1. *The Runner Assemblies with the Different Number of Blades*

The runner with flat blades had a circular hub of diameter also taken from Edeoja et al. (2015b) with 10 blades equally spaced around its periphery. The blades were detachable from the hub to enable adjustment laterally so that the test can be carried out at different blade angles. The runner with the adjustable flat blades is shown in Figure 2.

Figure 2. *The Adjustable Flat Blade Runner Assembly*

The runner with varying hub to blade ratios also had 10 v-blades based on the recommendations of Edeoja et al. (2016c). Five runners were fabricated with varying length of blades and sizes of hub attached to them. The hub to blade ratios of 0.7, 0.65, 0.55, 0.4 and 0.3 were selected around the approximate value of 0.55 reported in literature. Figure 3 shows the fabricated runners with the different hub to blade ratios.

Figure 3. *The Runner Assemblies with Different Hub to Blade Ratios*



The penstock outlets used were obtained by reducing 76.2 mm diameter to 15, 17.5, 20, 22.5 and 25 mm. The choice of 76.2 mm and reduction to the diameters selected was based on previous aspects of this work reported by (Edeoja and Awuniji 2017, Ipilakyya et al. 2017, Edeoja et al. 2016a). The penstock outlets used for the study are shown in Figure 4.

Figure 4. *The Penstock Outlets used for the Study*

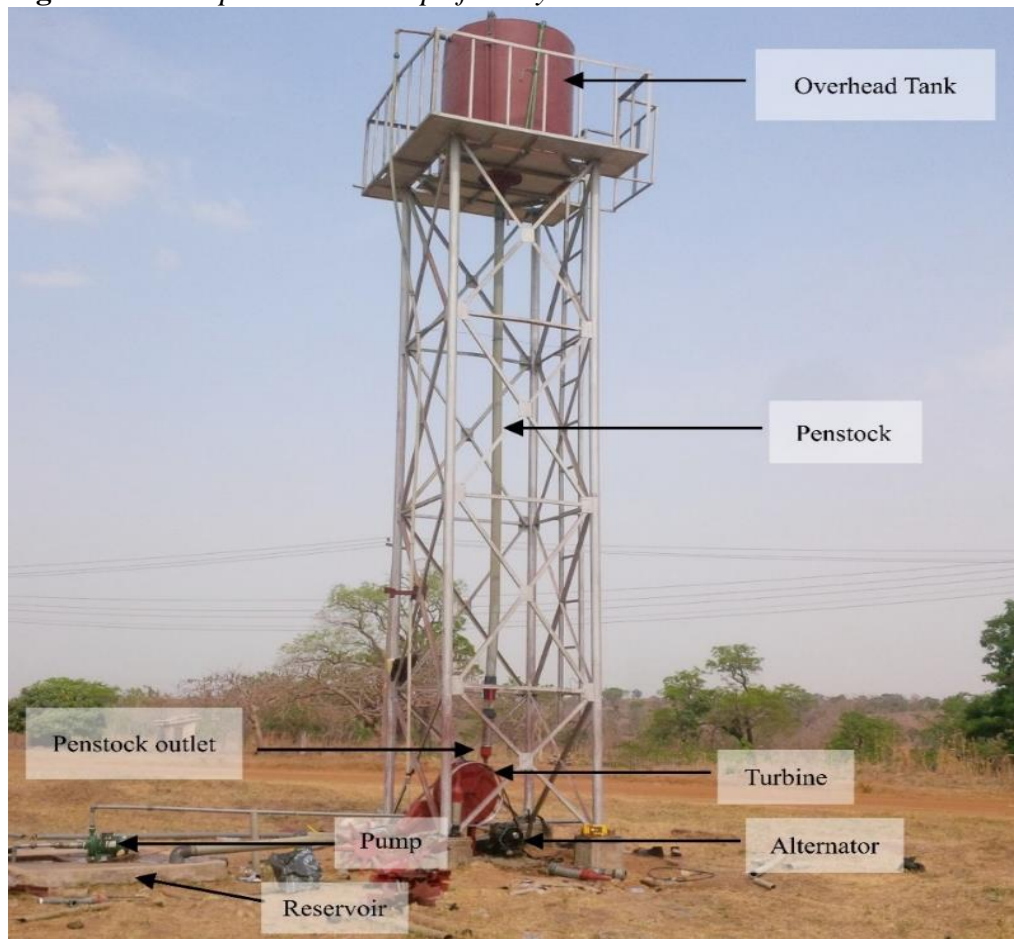


Each of the runners was clamped to the shaft flange with four M10 bolts and mounted in between two bearings and seals on the already existing turbine casing and covered to allow free spinning of the shaft and prevent leakages from the turbine one after the other. Some grease was also applied to the bearings to reduce

friction. The turbine cover was then secured in place with M14 and M13 bolts and the turbine pulley of about 605 mm diameter mounted on the 20 mm shaft. The upper and lower ends of the 76.2 mm PVC penstock were then connected to the overhead tank and the outlet respectively. Care was taken to align the turbine runner, casing and the penstock outlet so as to ensure a good clearance of about 15 mm. The turbine was then coupled to a 3.9 kVA alternator by means of a toothed v-belt drive onto a 50 mm pulley mounted on the shaft in a ratio of about 12:1.

The experimental set up for this study consists of a 1 Hp, 3-10.8 m³/h pump and the locally fabricated turbine connected in a closed loop with PVC piping as penstock, a 2000 litres overhead tank and a 3000 litres underground reservoir. Figure 5 shows a picture of the entire system.

Figure 5. *The Experimental Set up of the System*



The suction pipe of the pump draws water from the underground reservoir to the overhead tank to create a head. Water is then released from the overhead tank through the penstock and flows through the reduced diameter penstock outlet before impinging on the blades. The flow through the turbine is regulated using a gate valve installed before entry to the penstock. The water jet strikes the blades which are attached to the hub, therefore transferring its kinetic energy to the shaft

causing the rotary motion of the hub and the shaft assembly which develops a torque. The torque is then transferred to the alternator.

The experimentation was carried out in three batches. First, each number of v-blades was tested for each of the penstock outlets. Next, five lateral twist angles of the flat blades of 50, 55, 60, 75 and 90° were tested against the various penstock outlets. Finally, the runners with varying hub to blade ratio were then tested. For each test, water released by opening the gate valve through the penstock impinges on the blades. The blades are pushed tangentially by the falling water. The thrust produced by the water on the blades produces a torque on the shaft resulting in revolution of the runner. For each, a DT-2268 contact type tachometer was used to measure the rotational speeds of the turbine and alternator shaft speed in revolutions per minute. Also, the water levels in the reservoir and overhead tank before and after each test were monitored with the aid of a calibrated dip stick and each operation was timed using a stopwatch. The difference in water levels for the overhead tank was used to compute the flow rate. The water level in the overhead tank before the flow is used in computing the gross head. The major and minor losses were also computed. The hydraulic power was computed using the rotational speed of the turbine shaft. The results obtained were then correlated at 95% and a reliability test performed on them using Cronbach's alpha (CA).

Results

Figures 6 to 8 show the variation of the alternator shaft speed with number of v-blades, angle of twist of flat blades and hub to blade ratio respectively obtained for the respective penstock outlet diameters. Figures 9 to 11 show the variation of the alternator shaft speed with the penstock outlet diameter for the three other parameters.

Figures 12 to 14 show the variation of the system computed power with number v-blades, angle of twist of flat blades and hub to blade ratio respectively for the penstock outlet diameters. Figures 15 to 17 show the variation of the computed power with penstock outlet diameters for the three parameters.

Figure 6. Variation of Alternator Shaft Speed with Number of Blades for the Penstock Outlet Diameters

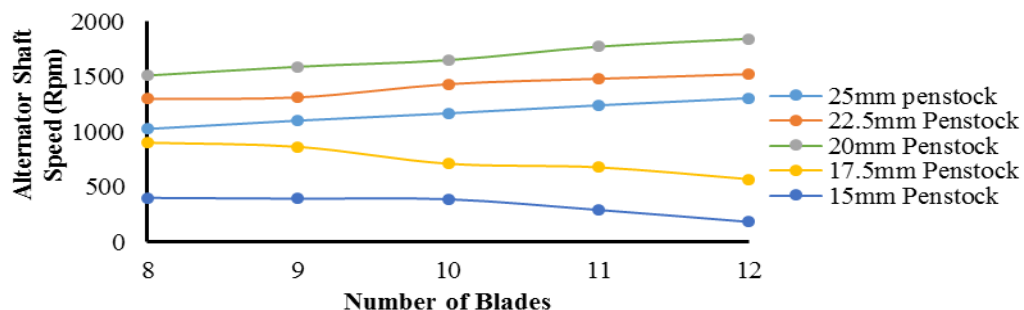


Figure 7. Variation of Alternator Shaft Speed with Blade Lateral Twist Angle

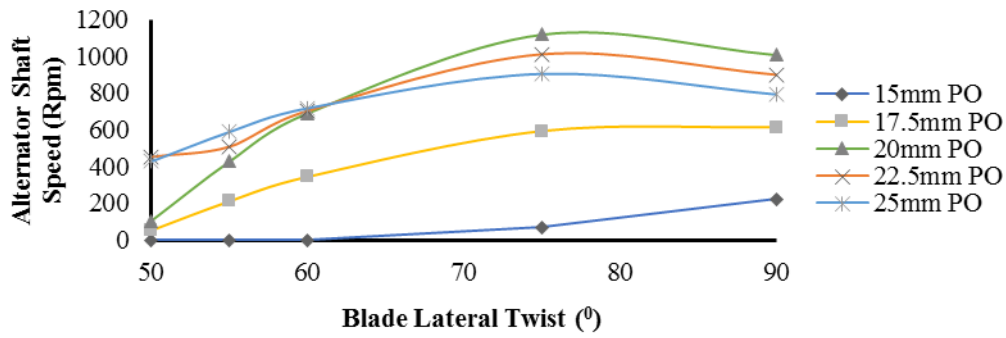


Figure 8. Variation of Alternator Shaft Speed with Turbine Hub to Blade Ratio

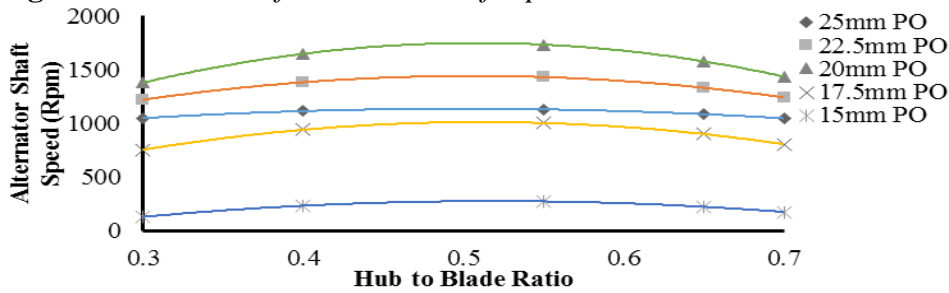


Figure 9. Variation of Alternator Shaft Speed with the Penstock Outlet Diameters for the Various Number of Blades

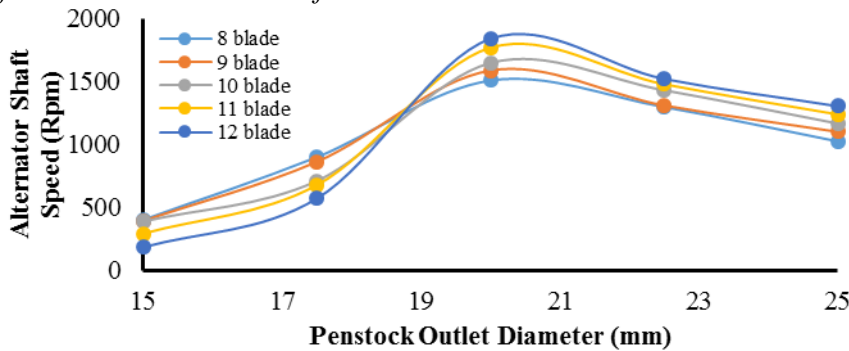


Figure 10. Variation of Alternator Shaft Speed with Penstock Outlet Diameters

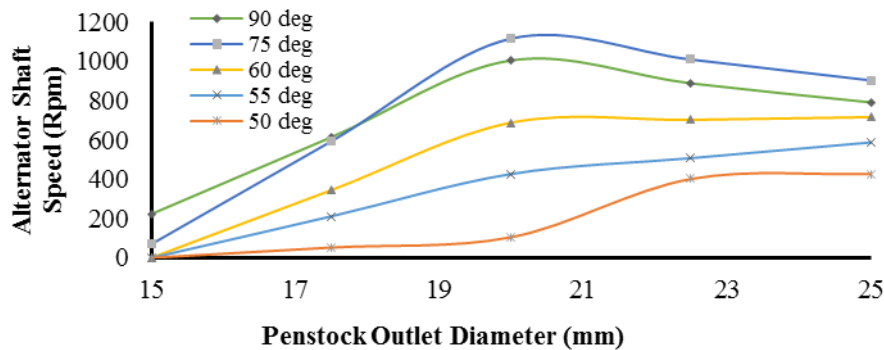


Figure 11. Variation of Alternator Shaft Speed with Penstock Outlet Diameter

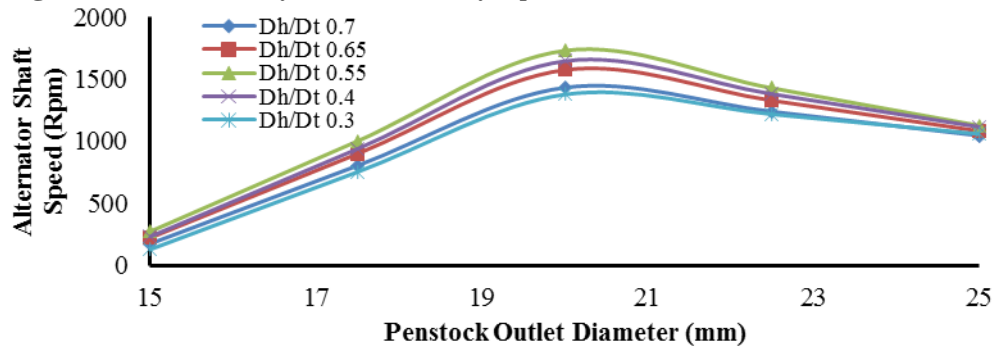


Figure 12. Variation of Computed Power with the Number of Blades for the Penstock Outlet Diameters

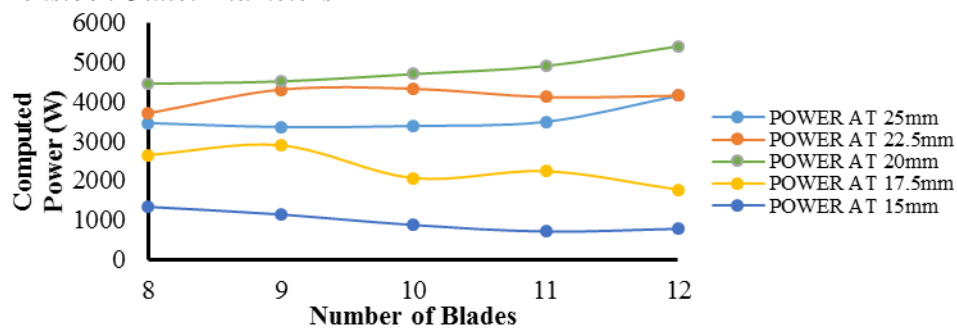


Figure 13. Variation of Computed Power against Blade Lateral Twist Angle

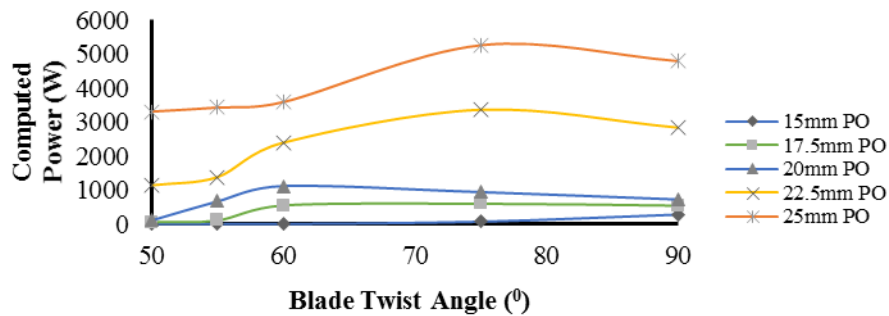


Figure 14. Variation of Computed Power with Turbine Hub to Blade Ratio

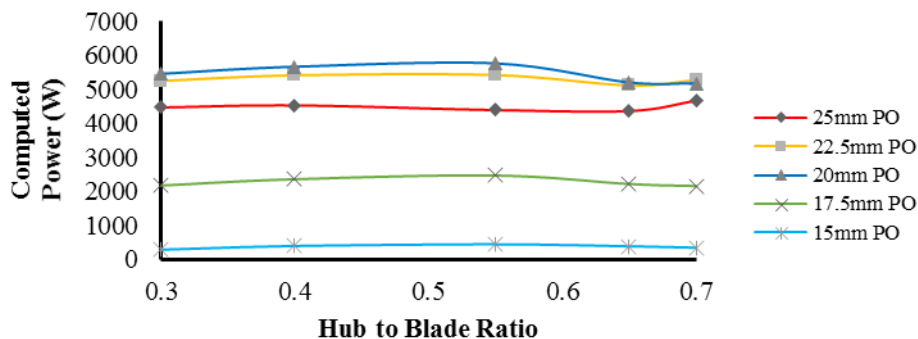


Figure 15. Variation of Computed Power with the Penstock Outlet Diameter for the Number of Blades

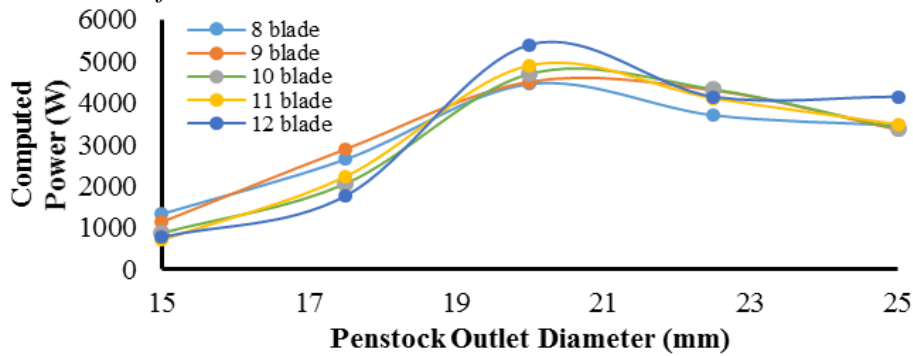


Figure 16. Variation of Computed Power with Penstock Outlet Diameter for the Blade Lateral Twist Angles

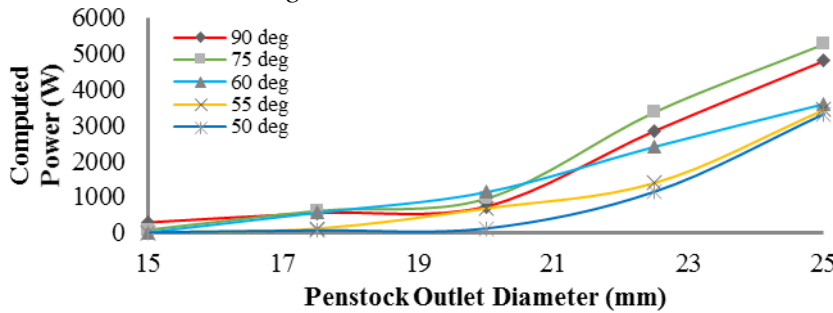
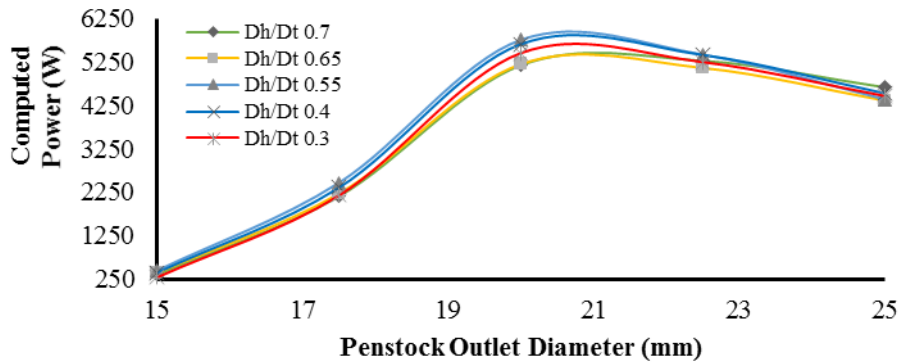


Figure 17. Variation of Computed Power with Penstock Outlet Diameter for the Hub to Blade Ratios



Tables 1 and 2 show the summary of the result of Pearson’s correlation test carried out on the data, while Tables 3 to 5 show the summary of the result of the reliability tests carried out on the data using Cronbach’s Alpha (CA). In the tables, apart from the abbreviations already encountered, N_T refers to the turbine shaft rotational speed, N the ideal or expected speed of the alternator shaft, % loss the percentage difference between the actual and ideal alternator shaft speeds and P the computed power.

Table 1. *P-Value of Relationship between the Parameters and Power*

Parameters	N	P (W)*
BHR	25	0.941
BTA	25	(-)0.263
NOB	25	0.958
N _T (Rpm)	75	0.000
N _A (Rpm)	75	0.000
N (Rpm)	75	0.000
% loss	75	(-)0.133

*(-) indicates negative correlation.

Table 2. *P-Value of Relationship between the Pairs of Parameters*

Parameters	N	N _T (Rpm)	N _A (Rpm)	N (Rpm)	% loss	P (W)
POD	75	0.000	0.000	0.000	(-)0.228	0.000
BHR	25	(-)0.916	(-)0.973	(-)0.827	0.861	0.941
BTA	25	(-)0.005	(-)0.004	(-)0.005	(-)0.152	(-)0.263
NOB	25	0.822	0.831	0.822	0.423	0.958
% loss	75	(-)0.345	(-)0.006	(-)0.781	-	(-)0.133

Table 3. *Reliability of the System on the Number of Blades (NOB) and Other Parameters*

Item	Cronbach's Alpha	CA if Item Deleted
P (W)	0.692	0.662
N _A (rpm)		0.499
N (Rpm)		0.501
% loss		0.724
N _T (rpm)		0.703
NOB		0.721

Table 4. *Reliability of the System on the Blade Hub Ratio and Other Parameters*

Item	Cronbach's Alpha	CA if Item Deleted
P(W)	0.631	0.628
N _A (rpm)		0.475
N (Rpm)		0.406
% loss		0.658
N _T (rpm)		0.638
BHR		0.657

Table 5. Reliability of the System on the Blade Twist Angle (BTA) and Other Parameters

Item	Cronbach's Alpha	CA if Item Deleted
P (W)	0.530	0.666
N_A (rpm)		0.384
N (Rpm)		0.299
% loss		0.548
N_T (rpm)		0.530
BTA		0.552

Discussion

Figure 6 to 8 confirm the general expectation that the alternator shaft speed (N_A) improves with increasing flow rate, a function of flow area, which favors the development of higher torques (Edeoja et al. 2016a, Derakhshan and Kasaiean 2012, Park et al. 2012, von Flotow 2012, Smith and Bush 2010). Also, it has been shown for this system that N_A increases with the number of blades (NOB) before deteriorating after about 10 to 12 blades (Edeoja et al. 2016c). Figure 6 shows that N_A steadily increased with NOB for the range of penstock outlet diameter (POD) of $20 \text{ mm} \leq POD \leq 25 \text{ mm}$ as against a decrease after $NOB = 9$ for $POD \leq 17.5 \text{ mm}$. The value for $POD = 20 \text{ mm}$ were generally the highest including the ones within the $20 \text{ mm} \leq POD \leq 25 \text{ mm}$ range. This confirms the tendency of flow acceleration increasing with area reduction until a turning point is attained depending on the initial area. The values for $POD = 22.5$ and 25 mm generally agree with the fact that larger diameters support higher flow rates resulting in large values of N_A (Tamrakar et al. 2015, Al Amin and Talukder 2014, At-Tasneem 2014, Martins and Sharma 2014, Sangal et al. 2013, Yassi and Hasemloo 2010). Hence, the combination of an optimum $POD = 20 \text{ mm}$ and increasing NOB favors the production of good torque and as a result improved N_A .

Figure 7 shows that the pattern of variation of N_A for the respective $PODs$ was not well defined below blade twist angle (BTA) of 60° . Apart from some likely errors of alignment, this could largely be attributed to insufficient blade surface area of blade available for the water jet to strike. For $BTA \geq 60^\circ$ however, for all the values of POD , N_A increased steadily with BTA , peaking around 75° before deteriorating. However, for $POD = 15 \text{ mm}$, N_A did not deteriorate because the reduced flow area was compensated for by the greater blade surface area available for interaction with the water jet. On the whole, BTA varied with N_A in the range $20 \text{ mm} \leq POD \leq 25 \text{ mm}$ in a similar fashion as the case with NOB vis a vis being highest for $POD = 20 \text{ mm}$ followed by 22.5 mm and the 25 mm . Hence, $BTA \geq 75^\circ$ and $POD = 20 \text{ mm}$ will favour larger values of N_A .

Figure 8 shows the variation of hub to blade ratio (HBR) with N_A . It also generally indicated that N_A was higher for the range $20 \text{ mm} \leq POD \leq 25 \text{ mm}$, with the values for $POD = 20 \text{ mm}$ being also highest followed by the others as before. Also, the general tendency was for N_A to peak at $HBR = 0.55$ which agrees with the range of values reported by several researchers (Pacayra et al. 2016,

Williamson et al. 2011, Simpson and Williams 2011, Sopian and Ab Razak 2009). This was not however significant for $POD = 25$ mm probably because the increased flow rate for the larger diameter outlet compensated for all the other values of HBR . Hence, $POD \geq 20$ mm and $HBR = 0.55$ favor the development of higher values of N_A .

Figures 9 to 11 display the variation of N_A with POD for the other three parameters. They generally agree with the foregoing discussions. They respectively show that 12 blades, $BTA \geq 75^\circ$ and $HBR = 0.55$ along with $POD = 20$ mm favour a good performance in terms of the N_A attained. On a general note, high values of N_A lead to larger power outputs. Hence, the combination of these parameters yielding high N_A should potentially produce large power output.

Figures 12 to 14 show the relationship between the system's computed power with NOB , BTA and HBR for the various $PODs$. The figures bear some resemblance to Figures 6 to 8 expectedly because the power generated in a conventional hydropower system depends more or less directly on N_A (Alnakhilani et al. 2015, Ridzuan et al. 2015, Chukwunke et al. 2014, Yadav and Chauhan, 2014, Katre and Bapat 2014, Ho-yan 2012, Ho-yan 2011, Pengchang et al. 2006). In Figure 14, however, the variation of the computed power with BTA for $POD = 20$ mm did not resemble the pattern shown in Figure 8. This probably could have been as a result of some alignment and measurement errors. It was nonetheless above the trends for $POD \leq 17.5$ mm, thereby affirming that the range $20 \text{ mm} \leq POD \leq 25$ mm favors good system performance. Along with this range of POD , Figure 13 shows that $NOB = 12$ yielded the highest computed power of > 5000 W. Also, $BTA \approx 75^\circ$ gave the highest computed power for the same range as shown in Figure 14. Figure 15 also indicated slightly that $HBR = 0.55$ produced the highest power output though for all values of HBR , the computed power for the range $20 \text{ mm} \leq POD \leq 22.5$ mm were all > 5000 W.

Figures 15 to 17 show the relationship between the computed power and the $PODs$ for the various NOB , BTA and HBR . They further strengthen the findings reflected in Figures 12 to 14. Hence, for the system, the condition that $20 \text{ mm} \leq POD \leq 22.5$ mm, $NOB = 12$, $BTA \geq 75^\circ$ and $HBR = 0.55$, favor large power generation. For the ongoing development of a clean, decentralized and highly simplified energy system, these findings represent very good indications for the actual implementation for end user applications.

Tables 1 and 2 indicate that BHR , BTA , NOB and % loss have no statistically significant relationship with (or effect on) the power of the system with $p > 0.05$. However, POD has a highly significant effect on the power with $p < 0.05$. Furthermore, each of POD and BTA individually has a highly significant relationship with each of N_T , N_A and N with $p > 0.05$ for each case which in turn individually has a highly significant relationship with power ($p < 0.05$). It is noteworthy that the relationship of BTA with the N-parameters is negative such that as one increases the other is expected to decrease. On the other hand, each of BHR and NOB individually has no statistically significant effect on the N-parameters and % loss ($p > 0.05$) and hence, on the power of the system. % loss has no significant relationship with any of the parameters except N_A . Meanwhile, the relationship is negative such that the lower the former the higher the latter.

Hence, N_A is the most critical of all N-parameters, agreeing with what has been established earlier on in the discussion. High N_A is desired for high power and low % loss. In order of preference, high POD is desired for increasing both N_A and power followed by lowering BTA for increasing N_A . BHR and NOB have no statistically significant consequences at this level.

Cronbach's alpha (CA) is used to test the extent of reliability of the performance of the system on the parameters. When $CA > 0.05$, it means that a statistically highly significant reliability level exists. The value of CA when a parameter is removed from the system is also given as shown in Tables 3 to 5. From the tables, the performance of the system has a highly significant reliability on the NOB , BHR and BTA combined with other identical parameters because of their high CA values of 0.692, 0.631 and 0.530 respectively. This is indicated from the respective values of turbine and hence alternator shaft speeds. Low values of these parameter result in reduction in CA values. This means that the system performance most highly relies on the value of these parameters. Also, CA would be highly improved when % loss is reduced in the system. Hence, the performance least significantly relies on % losses and so, all effort must be made to remove % losses. However, since the CA value when each of NOB , BHR and BTA are respectively removed from the system is only higher for BTA than when % loss is removed in Table 5, it implies that the system performance relies more on BTA than % loss with the reverse is applicable for BHR and NOB . Hence, N_A and N are very critical to the performance of the system. They must not be removed. % loss must be removed from the system to improve the performance. Also, the performance of the system significantly relies on NOB , BHR and BTA . However, the reliability of the systems improves when either is removed from the system. On the whole, a perfect match exists between the conclusions drawn from the two tests.

Conclusions

Based on the results obtained from the study, the following conclusions can be drawn for further development of the system with a view of improving performance and achieving end user status for small scale power generation:

1. For the v-blades configuration this particular Pico-hydro system, a 20 mm penstock outlet diameter with a 12 blade runner is appropriate for use.
2. The combination of flat blade twist angles in the range $75^\circ \leq \theta < 90^\circ$ with penstock outlet diameters in the range > 20 mm have very good potential for use on the Pico hydropower system with possibility for scaling to suit specific requirements for system performance.
3. In addition to the issues raised, the study also confirms that the hub to blade ratio of 0.55 is appropriate for this system.

The findings strengthens the resolve to keep striving in order to actualize the target of adding this system as an end user energy solution which is clean,

environmentally benign and less vulnerable to sabotage into the energy mix in Nigeria. The following recommendations/suggestions are made for further improvement of the performance of the simplified Pico hydro system:

1. Turbine casings used should have adequate provision for the runner not to run through the water so that drag forces on it can be minimized.
2. The effects of water jet misalignments will be further reduced by incorporating provision(s) for such in further designs.
3. Larger diameter pipes should be used in transferring water to the overhead tank to sustain the flow circle at the expense of justifiable higher cost.
4. Larger and/or multiple reservoirs will also be explored to enhance the robustness of the system.
5. Lighter metals such as aluminum should be used in fabricating the runners and blades as heavier metals like mild steel add to the inertia and thus decrease turbine performance.
6. The option of hybridization with solar energy is very viable in the location of the work and will be explored with better access to funding.

Most importantly, a general awareness and technical understanding of successful Pico-hydro technology needs to be developed and fostered at the local and regional levels so that rural electrification projects can be boosted.

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